## AERMOD Version 13350 Low Wind Options: Sensitivity Analysis and Evaluation Update

Study conducted on behalf of:

- API for sensitivity analysis
- Lignite Energy Council for evaluation update



#### **Outline of Presentation**

- Purpose and objectives of this study for AERMOD low wind options
- Sensitivity Study Funded by API
  - Model Options Tested
  - Source Types Modeled for Flat and Complex Terrain
  - Results of Sensitivity Analysis
- Evaluation Study Funded by Lignite Energy Council
  - Models and Options Tested
  - Database Tested to Date
  - Results of Evaluation Tests to Date



#### Purpose and Objectives: Sensitivity Analysis

- Explore the sensitivity of the AERMOD low wind speed options for predicted impacts in both flat and complex terrain
- Tested for a variety of emission sources of interest to the American Petroleum Institute and their members
- 11 different source types were examined, ranging from tall buoyant point sources to low-level fugitive sources
- Examined types of sources significantly affected by use of the low wind options in AERMET and AERMOD
- NO₂ was the pollutant selected → assumed full conversion of NOx to NO₂
- Model setup was based on hypothetical locations, but used input parameters and building downwash (when applicable) from real model applications

A=COM

#### Model Configurations and Options for Sensitivity Analysis

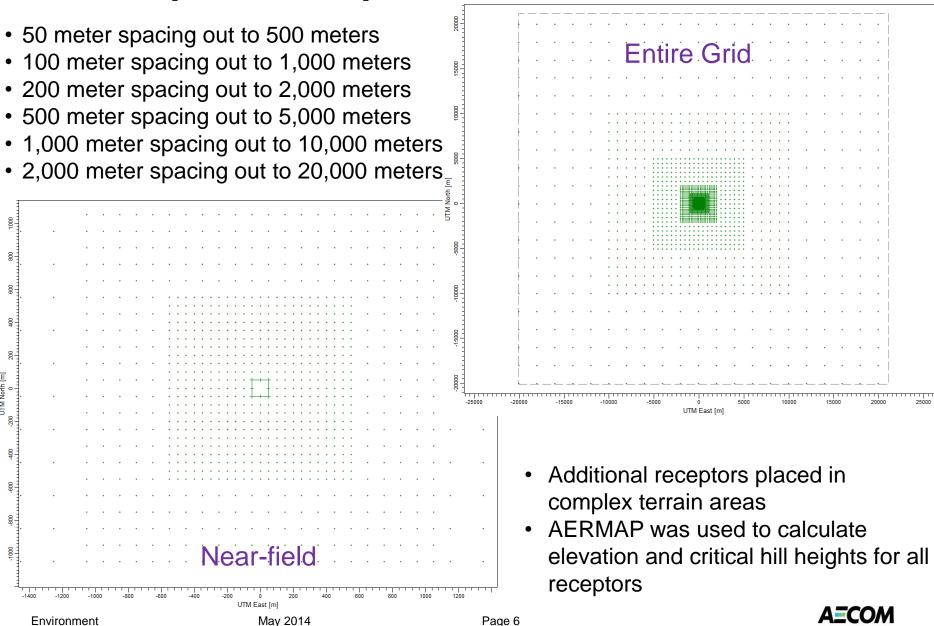
- AERMET/AERMOD Versions 13350 and 14134
- Three model configurations were run
  - AERMET/AERMOD all default
  - AERMET (Beta u\*) / AERMOD (default)
  - 3. AERMET (Beta u\*) / AERMOD (LOWWIND2)
- Each model configuration was run for each source in both flat and complex terrain
- Results from AERMOD versions 13350 and 14134 were the same



**Model Inputs: Source Types** 

| 111000    | imputs. Source Types   |            |                |                |          |
|-----------|--|------------|----------------|----------------|----------|
|           |  | Stack      | Stack          | Stack          | Stack    |
| Source ID | Source Description   | Height     | Temp           | Vel.           | Diameter |
| Source ID | Source Description   | (m)        | (K)            | (m/s)          | (m)      |
| FCC       | Source 1: a tall buoyant point source indicative of an FCC (fluid catalytic cracking) refinery source (including building downwash)                  | 54.0       | 561.0          | 49.1           | 2.0      |
| FLARE     | Source 2: a tall buoyant point source representing a flare (pseudo temp and velocity modeled to conserve buoyancy flux)                              | 75.6       | 1273.0         | 20.0           | 1.1      |
| REGENHTR  | Source 3: a tall buoyant point source indicative of a CCR (continuous catalytic regenerative reformer) refinery source (including building downwash) | 104.2      | 450.0          | 12.2           | 3.7      |
| GASTURB   | Source 4: a buoyant point source indicative of gas turbine at a compressor station (including building downwash)                                     | 13.7       | 777.0          | 41.6           | 1.2      |
| DIESENG   | Source 5: a short-stack horizontal elease point source indicative of a diesel generator (including building downwash)                                | 9.1        | 697.0          | 0.001          | 0.60     |
| DRILLRIG  | Source 6: a buoyant point source indicative of a drill rig (e.g., used at a fracking site, including building downwash)                              | 6.1        | 665.0          | 45.0           | 0.3      |
| LNGTURB   | Source 7: a combustion turbine source indicative of drilling or LNG facility operations.   | 13.7       | 777.0          | 30.0           | 3.0      |
| PNTTANK   | Source 8: a non-buoyant point source located on a tank (including downwash)  | 14.6       | ambient        | 0.001          | 0.001    |
| COMPRSTA  | Source 11: buoyant point source associated with a compressor station at a coal bed methane drilling site (including downwash)                        | 14.3       | 449.8          | 22.8           | 1.8      |
|           |  | Release    |                |                | Initial  |
|           |  | Height     | X-Dim.         | Y-Dim.         | Sigma-Z  |
|           |  | (m)        | (m)            | (m)            | (m)      |
| AREA      | Source 9: a ground-level area source   | 0.0        | 50.0           | 50.0           | 0.0      |
|           |  | Release    | Initial        | Initial        |          |
|           |  | Height (m) | Sigma-Y<br>(m) | Sigma-Z<br>(m) |          |
| ROADVOL   | Source 10: a volume source representing roadway traffic  | 10.0       | 14.0           | 16.0           |          |

**Model Inputs: Receptors** 

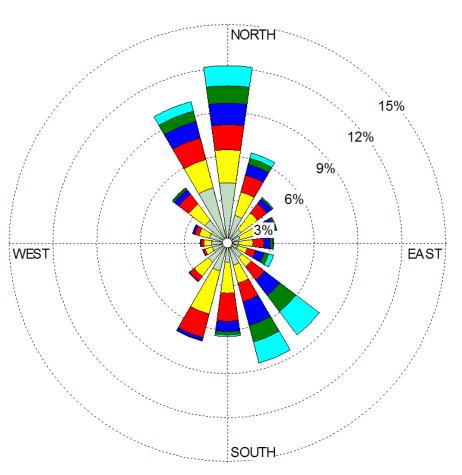


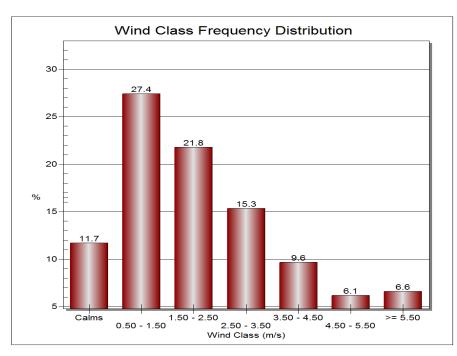
#### **Model Inputs: Meteorology**

- Two meteorological databases used in the study
- 1. Flat Terrain 2007-2011 from Pascagoula, Mississippi
- 2. Complex Terrain 2008-2012 from Page, Arizona
- Both meteorological databases feature a fairly large percentage of low wind speed hours
  - Winds < 1.5 m/s at least 25% of the time</li>
  - Winds < 2.5 m/s at least 60% of the time
- The location of the hypothetical sources in complex terrain was strategically positioned near (and upwind of) a major terrain feature

**AECOM** 

#### Flat Terrain Wind Rose and Frequency Distribution

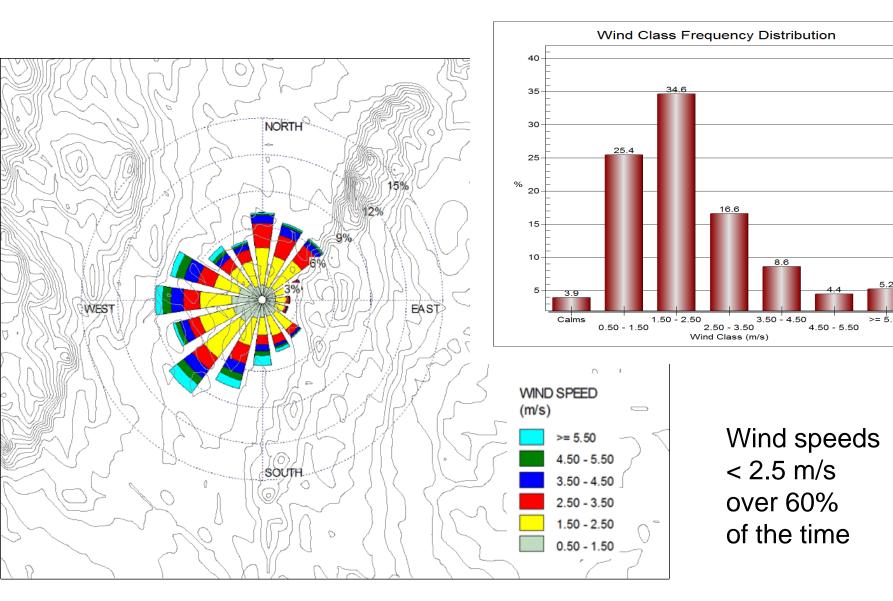




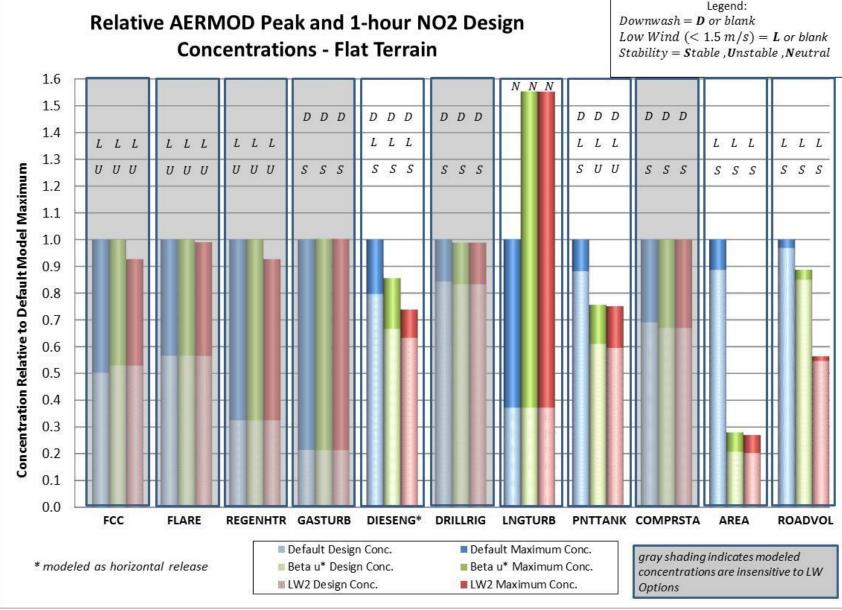
WIND SPEED (m/s) >= 5.50 4.50 - 5.50 3.50 - 4.50 2.50 - 3.50 1.50 - 2.50 0.50 - 1.50

Wind speeds < 2.5 m/s over 60% of the time

#### **Complex Terrain Wind Rose**



#### Model Relative Sensitivity Results: Flat Terrain



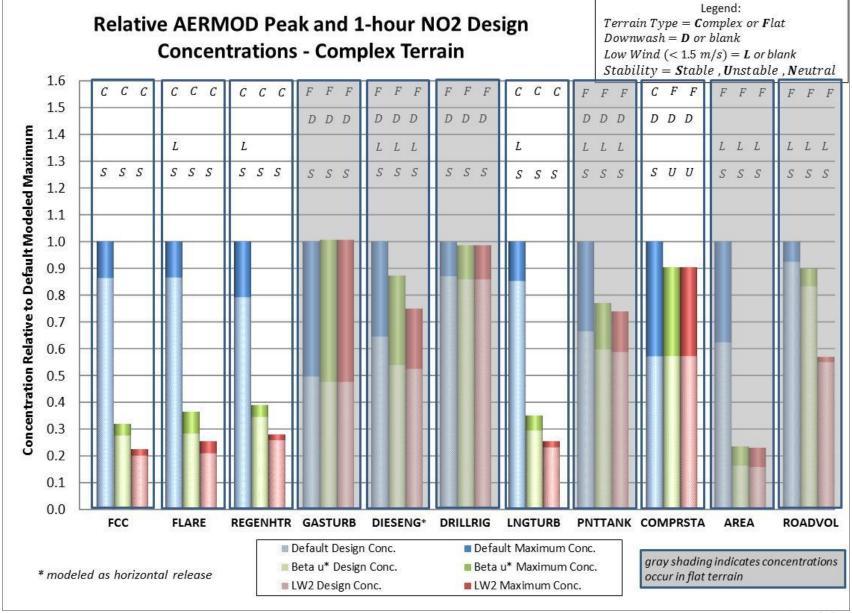
**AECOM** 

#### **AERMOD Low Wind Sensitivity – Flat Terrain**

- Tall buoyant stacks (FCC, FLARE, REGENHTR) were insensitive to the LW options - max impacts occur during unstable conditions
- Short buoyant stacks with downwash (DRILLRIG, COMPRSTA) insensitive to LW options - max impacts did not occur under light winds
- Short stacks without either momentum or buoyancy with downwash (DIESENG, PNTTANK) and fugitive sources are sensitive to LW options resulting in lower concentrations
  - max impacts occurred under light wind stable conditions
  - beta u\* increase mechanical mixing and vertical dispersion
- LNGTURB (short buoyant non-downwashing) source experienced a high wind "side effect" of the LW options
  - max impacts occur under high wind neutral conditions
  - use of beta u\* causes higher turbulence and plume touch down closer to the stack
- Low-level sources have peak impacts at low terrain near fenceline in complex terrain case as well

Environment May 2014 Page 11 AECOM

Model Relative Sensitivity Results: Complex Terrain

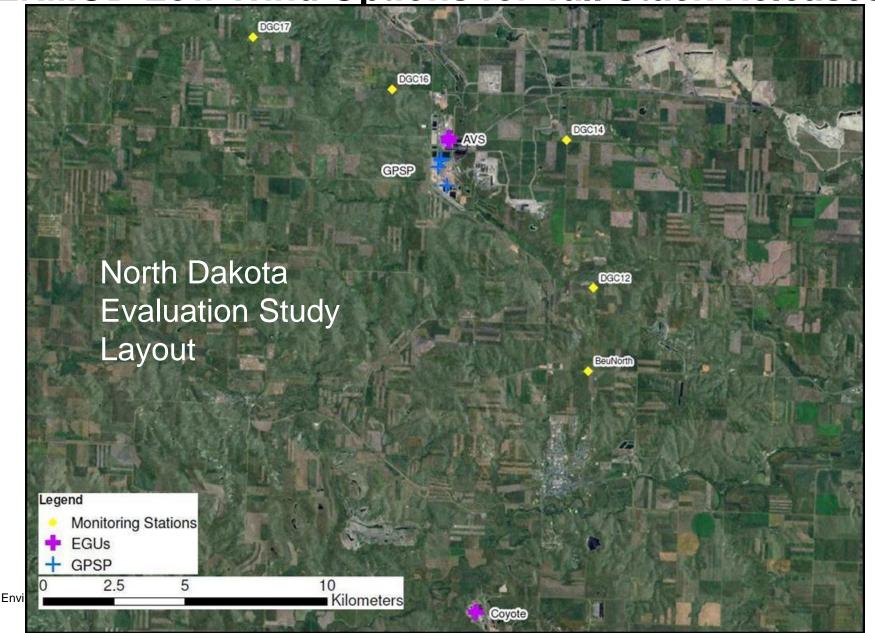


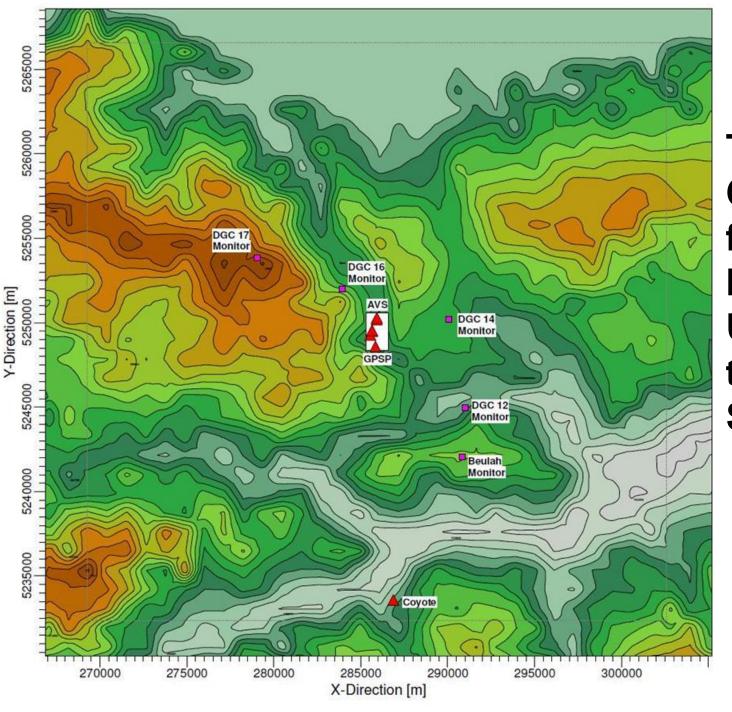
#### **AERMOD Low Wind Sensitivity – Complex Terrain**

- Tall buoyant stacks (FCC, FLARE, REGENHTR) are sensitive to the LW options in complex terrain
  - For default options, max impacts occur under light wind speed stable conditions
  - use of beta u\* increases effective wind speed, mechanical mixing, vertical dispersion, and plume rise; reduces predicted concentrations
  - use of LowWind2 also increases lateral dispersion and lower concentrations
- LNGTURB (short, non-downwashing) is sensitive to LW options
  - For default options, max impacts occur under light wind stable conditions
  - use of beta u\* increases mechanical mixing height and vertical dispersion
- COMPRSTA (short, downwashing) responds to LW options
  - For default options, max impact occurs under stable conditions (downwash)
  - Lower max impact for beta u\* option occurs in downwash during high wind unstable conditions

**AECO***M* 

Lignite Energy Council Evaluation of AERMOD Low Wind Options for Tall Stack Releases





# Terrain Contours for SO<sub>2</sub> Monitors Used in the ND Study

(10-m contour interval)



### Preliminary AERMOD Evaluation Results\* with Actual Hourly Emissions for North Dakota 4-year Database (07-10)

|         |          |          |               | AERMET with   |
|---------|----------|----------|---------------|---------------|
|         | Obs.     | AERMOD   |               | beta u*,      |
|         | Conc.    | 14134    |               | AERMOD with   |
|         | 4-yr Avg | with     | AERMET        | LOWWIND2      |
|         | 99th %   | default  | with beta u*, | with min      |
|         | Daily    | options: | default       | sigma-v =     |
|         | Max,     | Pre/obs  | AERMOD:       | 0.5 m/s:      |
| Monitor | μg/m³    | ratio    | Pre/obs ratio | Pre/obs ratio |
| DGC #12 | 91.52    | 1.28     | 1.28          | 1.05          |
| DGC #14 | 95.00    | 1.45     | 1.45          | 1.05          |
| DGC #16 | 79.58    | 2.00     | 2.00          | 1.58          |
| DGC #17 | 83.76    | 2.07     | 1.49          | 1.29          |
| Beulah  | 93.37    | 1.31     | 1.31          | 1.01          |

<sup>\*</sup> Note: assumes SO<sub>2</sub> background of 10 μg/m<sup>3</sup>

#### **Conclusions**

- This study reports sensitivity and field evaluation results for low wind options in AERMET/AERMOD
- Sensitivity was tested for 11 different source types
- In flat terrain, this option is important for low-level, nonbuoyant source types, and not for tall, buoyant stacks
- In complex terrain, this option is very important for tall, buoyant stack releases
- Low wind speed evaluations are underway for real-world field databases featuring tall, buoyant stacks: ND, Gibson
- For the North Dakota database, low wind options lead to better AERMOD performance, especially for the elevated terrain monitor. SCICHEM does well for this database.